

# Lesson 14: NEMA Designs and Induction Motor Nameplate Data

ET 332b

Ac Motors, Generators and Power Systems

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## Learning Objectives

After this presentation you will be able to:

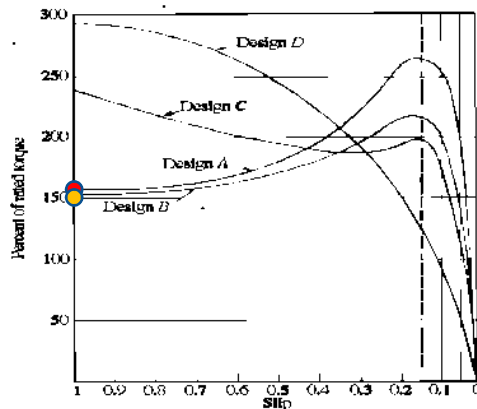
- List the characteristics of NEMA Design motors.
- Identify and interpret motor nameplate data.
- Use kVA codes to compute motor starting currents.
- Explain the effects of reduced motor voltage and frequency on machine performance.
- Compute the changes in motor speed and torque when voltage and frequency change.

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# NEMA Motor Designs

Different motor conductor designs given different rotor resistances, which gives different motor characteristics



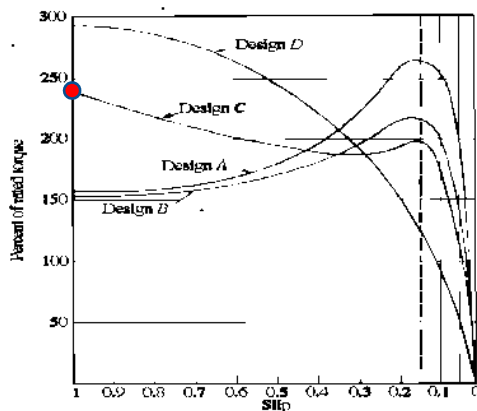
**Design A** - Starting torque 150% rated; breakdown torque 275% Starting current 7-10 times rated current

**Design B** - Starting torque approx. 150% rated; breakdown torque 225%; starting current < 6.4 times rated. Most commonly used motor design

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# NEMA Motor Designs



**Design C** - High starting torque motors; starting torque 240% to 275% of rated; starting I < 6.4 time I rated

**Design D** - High slip motors. Very high starting torques 275-300% of rated. Speed operates at 85-95% rated; slip 5-15%. Used to start high inertial loads Very low starting current, near rated at start.

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## Motor Nameplate Data

**Nominal Efficiency** - minimum efficiency that is guaranteed for design class. Given for one value of output - rated

**Design Letter** - indicates NEMA design type A, B, C, D

**Service Factor** - (S.F.) number that indicates the maximum permissible loading

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## Motor Nameplate Data

**Insulation Class** - specifies maximum allowable temperature rise for motor windings

**Code Letter** - means of determining the expected locked-rotor inrush current at rated voltage and rated frequency

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## Motor Nameplate Data

Code Letter kVA Table

Code Letter	kVA/hp	Code Letter	kVA/hp
A	0-3.15	K	8.0-9.0
B	3.15-3.55	L	9.0-10.0
C	3.55-4.0	M	10-11.2
D	4.0-4.5	N	11.2-12.5
E	4.5-5.0	P	12.5-14.0
F	5.0-5.6	R	14.0-16.0
G	5.6-6.3	S	16.0-18.0
H	6.3-7.1	T	18.0-20.0
J	7.1-8.0	U	20-22.4
		V	>22.4

Above can be used to compute the range of starting currents

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## Starting Current kVA Codes

Use kVA codes to find the range of motor starting currents

$$\text{kVA} \cdot \text{hp} \cdot 1000 = \sqrt{3} \cdot V_{LL} \cdot I_L$$

Where:  $V_{LL}$  = line-to-line voltage applied to motor terminals  
 $I_L$  = line value of starting current.  
 hp = rated motor horsepower

kVA comes from given table

Example: G = 5.6-6.3 kVA/hp

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## Starting Current kVA Codes

**Example 14-1:** A NEMA design motor is rated at 150 hp at 460, 60 Hz. It has a rated current of 163 A and a nominal efficiency of 96.2%. The locked rotor code is G. Find the range of starting current that can be expected from this machine.

Range for code G 5.6-6.3 kVA/hp

$$\text{Low value of kVA} = 5.6 \cdot \left( \frac{\text{kVA}}{\text{hp}} \right) \cdot 150 \cdot \text{hp} = 840 \text{ kVA}$$

$$\text{High value of kVA} = 6.3 \cdot \left( \frac{\text{kVA}}{\text{hp}} \right) \cdot 150 \cdot \text{hp} = 945 \text{ kVA} \quad V_L := 460 \cdot V$$

Low value of starting current

High value of starting current

$$I_{lr} := \frac{840 \cdot \text{kVA} \cdot 1000}{\sqrt{3} \cdot 460 \cdot V}$$

$$I_{lr} = 1054.3 \text{ A}$$

$$I_{lr} := \frac{945 \cdot \text{kVA} \cdot 1000}{\sqrt{3} \cdot 460 \cdot V}$$

$$I_{lr} = 1186.1 \text{ A}$$

$$\text{Range } 1054.3 \leq I_{lr} \leq 1186.1$$

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## Effects of Reduced Terminal Voltage and Frequency

Machines can operate +/- 10% of rated terminal voltage without significant change in characteristics.

Motor rated voltage 460 V, Supply voltage 480 V

$$\%V = \left( \frac{V_{\text{supply}}}{V_{\text{rated}}} \right) \cdot 100\%$$

$$\%V = \left( \frac{480 \text{ V}}{460 \text{ V}} \right) \cdot 100\%$$

$$\%V = 104\%$$



Generally must change both voltage and frequency to maintain torque-speed characteristic (constant flux) (Can't vary terminal voltage for speed control)

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## Effects of Changing Voltage and Frequency on Torque

Use the following empirical formula

$$T_D = k \cdot \left( \frac{V^2 \cdot s}{f} \right) \quad s \leq 0.03$$

Where:  $T_D$  = motor developed torque  
 $V$  = motor terminal voltage  
 $f$  = motor operating frequency  
 $s$  = per unit slip  
 $k$  = proportionality constant

Torque proportional to  $V^2$ ,  $s$  and inversely proportional to  $f$

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**Example 14-2:** A 3-phase 460 V, 20 HP, 60 Hz, 4 pole motor drives a constant torque load at rated shaft power at rated voltage, and frequency. The motor speed under these conditions is 1762 RPM. A system disturbance lowers the motor voltage by 10% and the system frequency by 6%. Find: a.) the new motor speed; b.) the new shaft power. Assume that the mechanical losses ( $P_{fw}$  and  $P_{stray}$ ) are constant.

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## Example 14-2 Solution (1)

Define equations

$$T_{D1} = k \left[ \frac{V_1^2 s_1}{f_1} \right] \quad T_{D2} = k \left[ \frac{V_2^2 s_2}{f_2} \right]$$

FOR CONSTANT TORQUE LOAD

$$T_{D1} = T_{D2}$$

OTHER KNOWN VALUES

$$f_1 = 60 \text{ Hz} \quad V_1 = 460 \text{ V} \quad n_{r1} = 1762 \text{ RPM} \quad P = 4$$

$$V_2 = (1 - 0.1) \cdot 460 \text{ V} = 414 \text{ V}$$

For 10% voltage reduction

$$6\% \text{ frequency reduction} \quad f_2 = (1 - 0.06)(60 \text{ Hz}) = 56.4 \text{ Hz}$$

Find  $s_1$ . This requires synchronous speed

$$n_{s1} = \frac{120 f_1}{P}$$

$$n_{s1} = \frac{120(60 \text{ Hz})}{4} = 1800 \text{ RPM}$$

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## Example 14-2 Solution (2)

Compute slip for 1<sup>st</sup> case

$$s_1 = \frac{n_{s1} - n_{r1}}{n_{s1}} = \frac{(1800 - 1762) \text{ RPM}}{1800 \text{ RPM}}$$

$$s_1 = 0.0211$$

Constant torque load so equate torques

$$\text{WITH } T_{D1} = T_{D2} \\ k \left[ \frac{V_1^2 s_1}{f_1} \right] = k \left[ \frac{V_2^2 s_2}{f_2} \right]$$

$$\frac{V_1^2 s_1}{f_1} = \frac{V_2^2 s_2}{f_2}$$

Solve for  $s_2$

$$\frac{f_2 V_1^2 s_1}{V_2^2 f_1} = s_2$$

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### Example 14-2 Solution (3)

Compute the value of  $s_2$

$$\frac{(56.4 \text{ Hz})(400)^2 (0.0211)}{(414)^2 (60 \text{ Hz})} = s_2$$

$$0.0245 = s_2$$

USING PER UNIT QUANTITIES

$$f_1 = \text{Rated} = 1.0 \quad V_1 = \text{rated} = 1.0$$

$$f_2 = 1 - 0.06 = 0.94 \quad V_2 = 1.0 - 0.1 = 0.9$$

Per Unit produces the same result

$$\frac{(0.94)(1.0)^2 (0.0211)}{(0.9)^2 (1.0)} = s_2$$

$$0.0245 = s_2$$

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### Example 14-2 Solution (4)

Need synchronous speed for second case

Find  $n_{s2}$

$$n_{s2} = \frac{120 f_2}{P} = \frac{120 (56.4 \text{ Hz})}{4}$$

$$n_{s2} = 1692 \text{ RPM}$$

Now compute the new motor speed

$$n_{r2} = (1 - s_2) n_{s2} = (1 - 0.0245)(1692 \text{ RPM})$$

$$n_{r2} = 1650.5 \text{ RPM}$$

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## Example 14-2 Solution (5)

Solve part b.  $P_1$  = rated horsepower = 20 hp

$T_{s1}$  = shaft torque state 1

$T_{s2}$  = shaft torque state 2

For constant torque load  $T_{s1} = T_{s2}$

For  $T$  (lbf-ft)

$$\frac{P_1}{P_2} = \frac{\frac{T_{s1} n_{r1}}{5252}}{\frac{T_{s2} n_{r2}}{5252}} \quad \text{SINCE} \quad T_{s1} = T_{s2}$$

$$\frac{P_1}{P_2} = \frac{n_{r1}}{n_{r2}} \Rightarrow P_1 = \frac{n_{r1}}{n_{r2}} P_2$$

$$P_2 = \left[ \frac{n_{r2}}{n_{r1}} \right] P_1$$

$$P_2 = \left[ \frac{1762 \text{ RPM}}{1650.5 \text{ RPM}} \right] 20 \text{ hp}$$

$$P_2 = 18.73 \text{ hp}$$

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## End Lesson 14: NEMA Designs and Induction Motor Nameplate Data

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